

The Annual Rv Method for Site-Level Green Infrastructure

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Amec Foster Wheeler

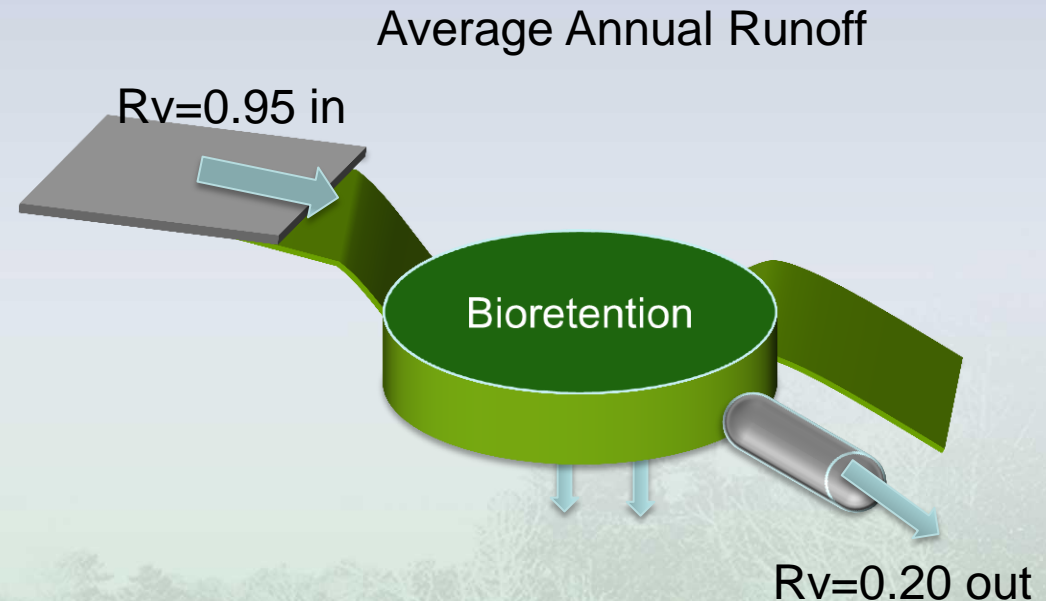
Nashville & Knoxville, TN

*“Everything should be made as simple
as possible, but not simpler”*

Albert Einstein

The Gist of the Rv Method

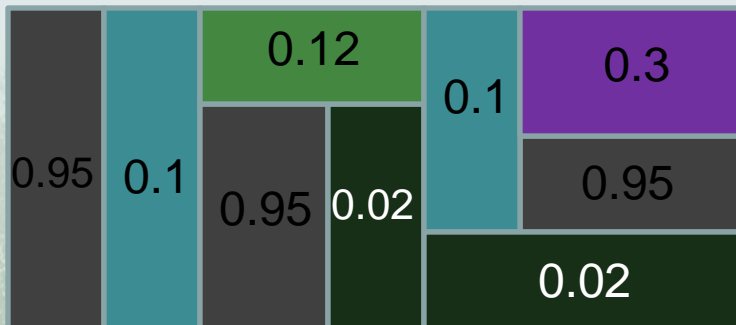
1. Average annual runoff ratio (Rv) must hit a target value
2. Each land use has an Rv estimated
3. Flow thorough natural and structural GIPs reduces the Rv from the combination



The weighted sum of Rv's for each land use or combination must be less than the target value.

So this ends up looking just like
a C Factor or CN calculation on a site:

The land-use weighted Rv must be ≤ 0.20



$$\frac{\sum Rv_i * A_i}{A_{\text{site}}} \leq 0.20$$

Brief overview of why and how we derived the method.



...built and maintained to infiltrate, evapotranspire, harvest and/or use... the stormwater runoff generated at a site by the first inch of every rainfall event preceded by 72 hours of no measurable precipitation... no runoff

Unintended Consequences

- If we take this literally we would have to create storage space for 1" rain every time thus reducing natural treatment's value
- Capturing the first inch after 72 HR IEPD would only capture 54% of the rainfall in Nashville
- We felt these were unintended consequences of the language at the time

MWS Overall Approach

Do a voluntary program to introduce Green Infrastructure to our community two years ahead of its mandatory use.

Develop an approach that has a high probability of success.

Remember there was no technical guidance at the time.

So...we talked to some smart old friends about lessons learned.



Dr. Rob Traver



Dr. Barrett Kays



Dr. Bob Pitt



Dr. Bill Hunt

A few key ideas:

- Urban soils are very complex and are never mapped – use a constant and conservative infiltration rate
- Modeling of individual urban sites is overly complex and highly inaccurate for every day use – you will never have enough data
- Instantaneous pollution is not normally the problem why not use a longer term metric
- In tight soils or bedrock underdrains mimic natural hydrology
- Capture depth requirements can produce overdesign and grey solutions – “Kerplunk” design
- Your method should integrate natural vegetation and processes in a non-artificial way
- Promote natural, low maintenance approaches as a priority

A man with grey hair, wearing a light green button-down shirt and blue jeans, is crouching on a rocky stream bed. He is holding a dark, irregularly shaped object in his hands, looking at it intently. The background shows a shallow stream with white, foamy water flowing over rocks, surrounded by green foliage and trees. A blue speech bubble is positioned in the upper right corner of the image.

Complicated
spreadsheets...
No kidding.

Tom Schueler Chesapeake Bay, Center for Watershed
Protection and Washington DC Stormwater program



How we think
GI gets built

How GI
actually gets
built

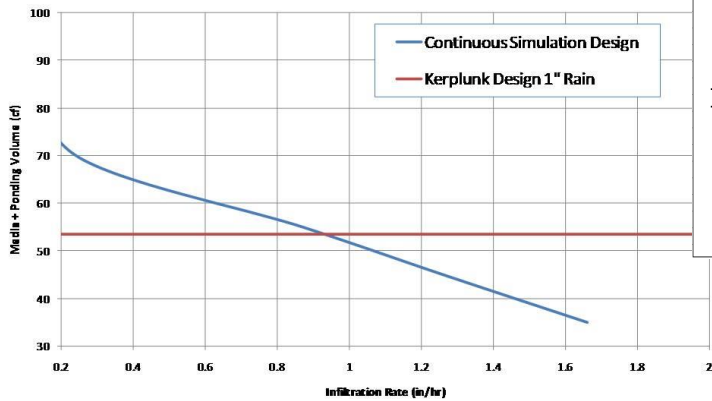


In Summary

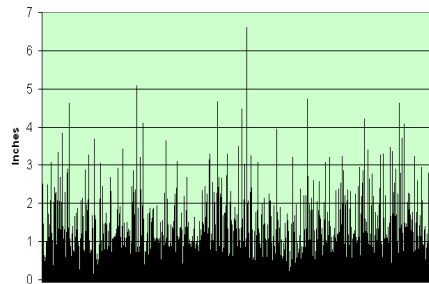
- **We can be smarter than we are wise**
- **You would be far better off creating a framework that:**
 - realistically reflects the urban facts on the ground
 - Balances hydrologic mimicry and an ability to capture and treat about the right volume
 - relatively easy to use given the experience and skills of the common user



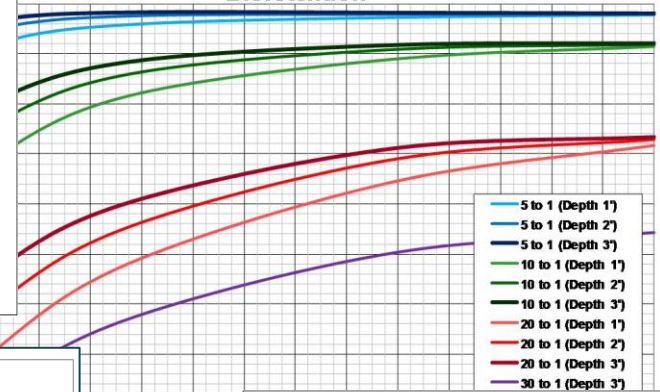
Bioinfiltration: Kerplunk vs. Continuous Simulation Nashville, TN 1" depth \approx 80% Capture



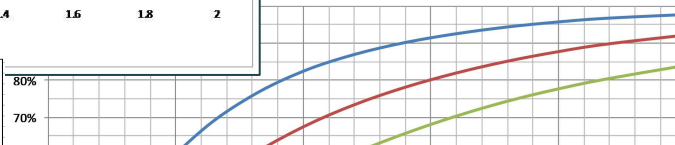
Nashville Daily Rainfall 1/1/1948-8/31/2009



Bioretention

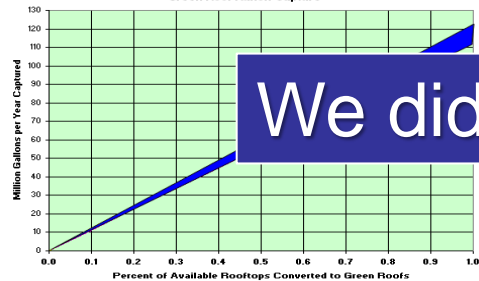


Water Capture Analysis

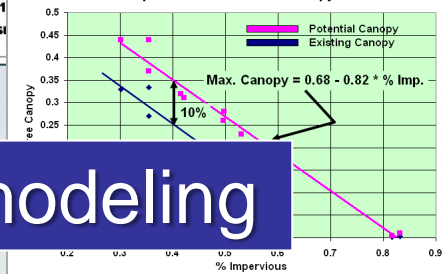


We did a lot of investigation and modeling

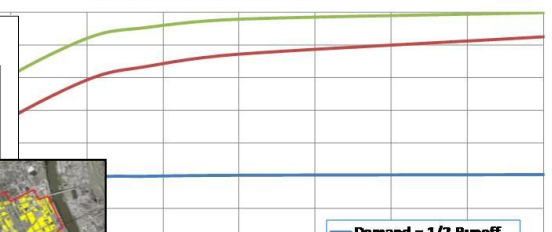
CSS Area of Nashville Green Roof Runoff Capture



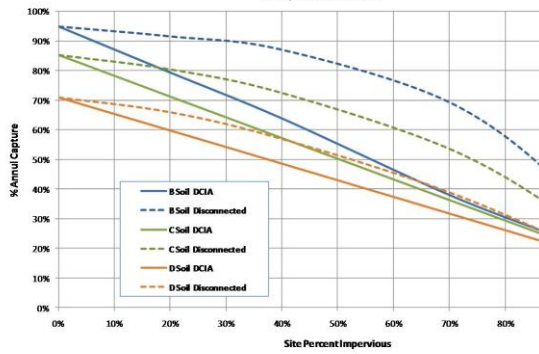
Imperviousness vs. Tree Canopy



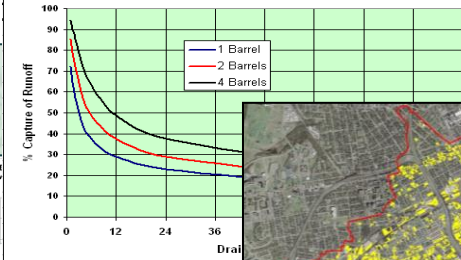
Cistern Demand and Sizing per 1,000 sf of roof, 0.8 loss coefficient



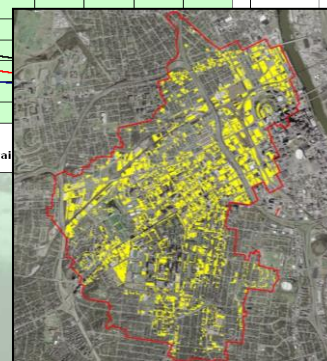
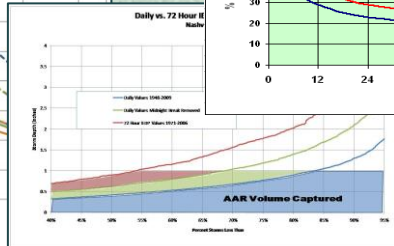
Annual Rainfall Capture Hourly Rainfall 1971-2006



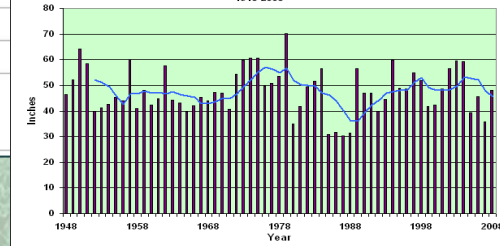
Rain Barrel Performance 1,000 SF Roof, 0.8 Runoff Coefficient



Daily vs. 72 Hour R



Annual Rainfall Nashville Airport 1948-2008



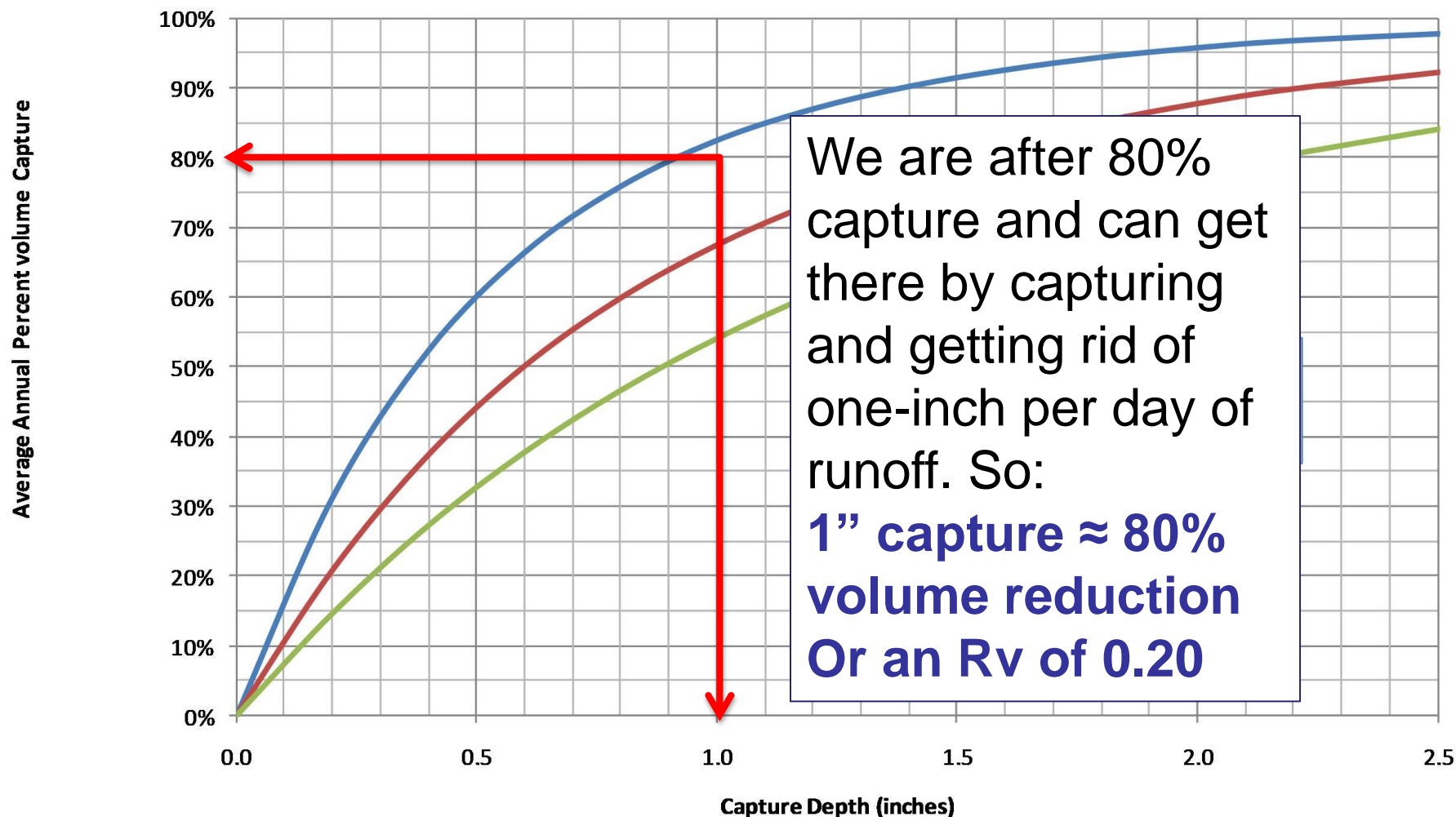
Right – so you’re saying if all my developers can do continuous simulation then I can use this method?

**And that is simpler
how again?**



1" Storm Volume Captured: 80%

Volume Capture Analysis

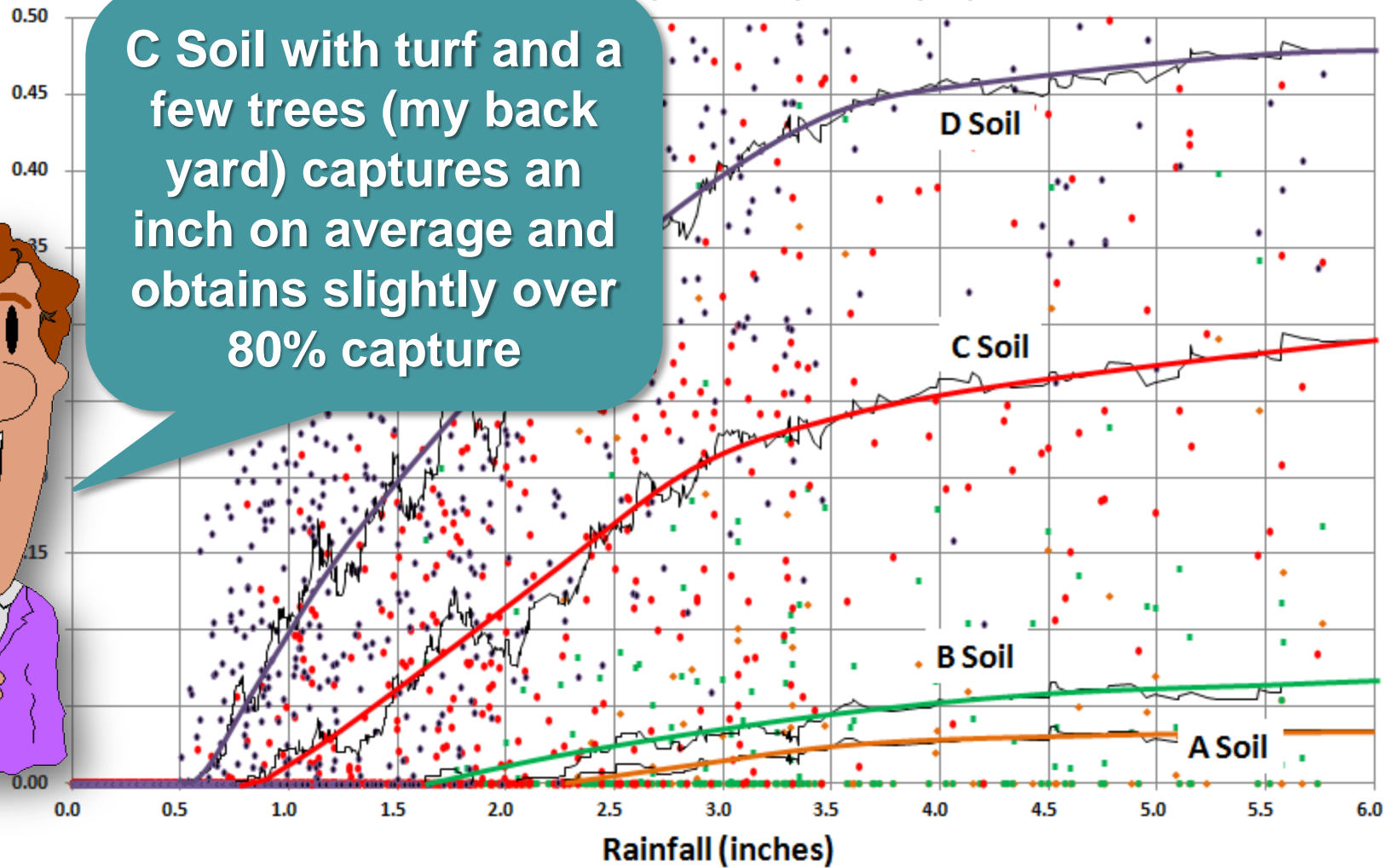




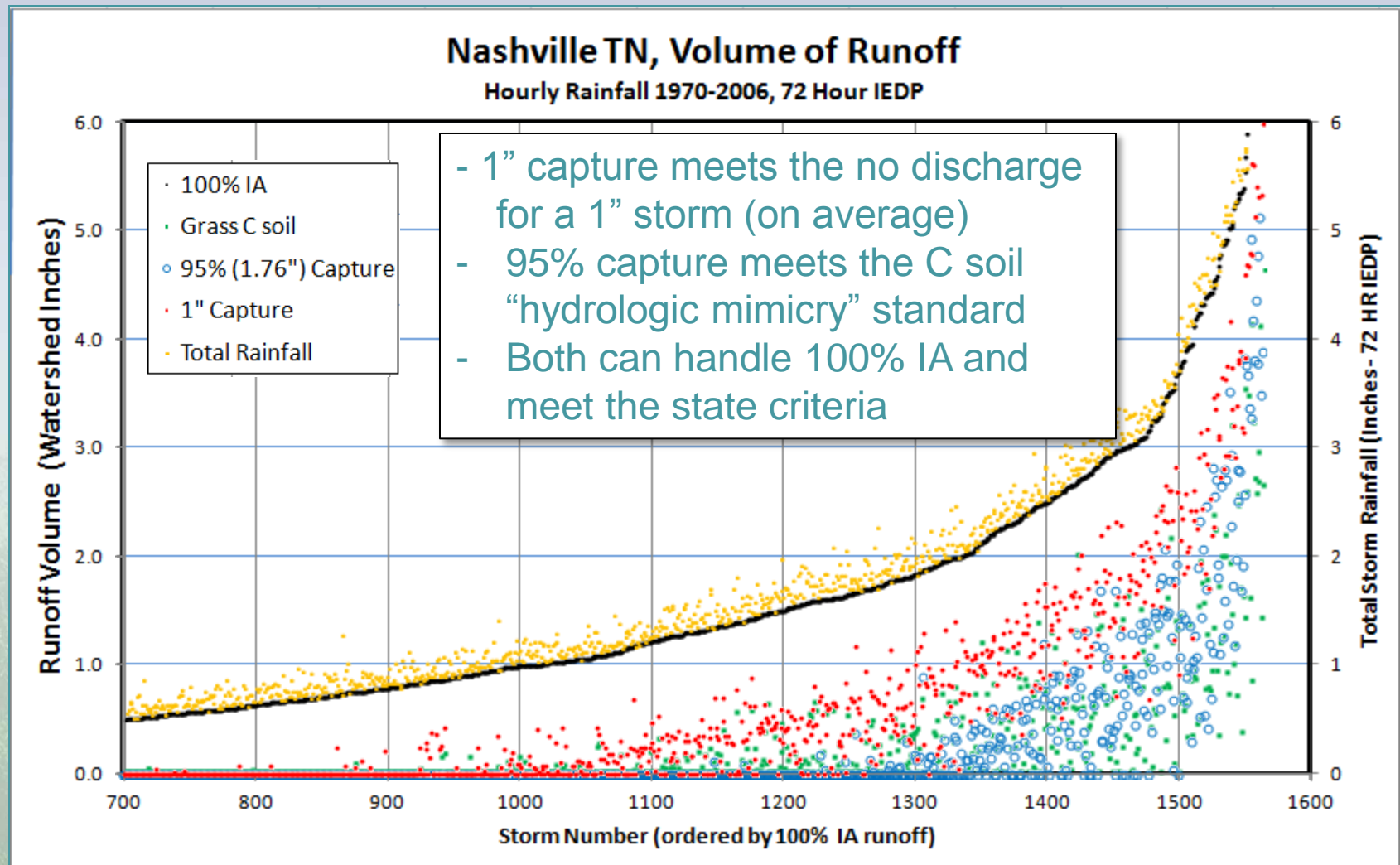
Rainfall-Runoff Data & Trend Lines Four Soil Types

Hourly Rainfall 1971-2006, 72 HR IEDP, Nashville, TN,

C Soil with turf and a few trees (my back yard) captures an inch on average and obtains slightly over 80% capture



Green Infrastructure Bioretention Runoff Volume Reduction Effectiveness



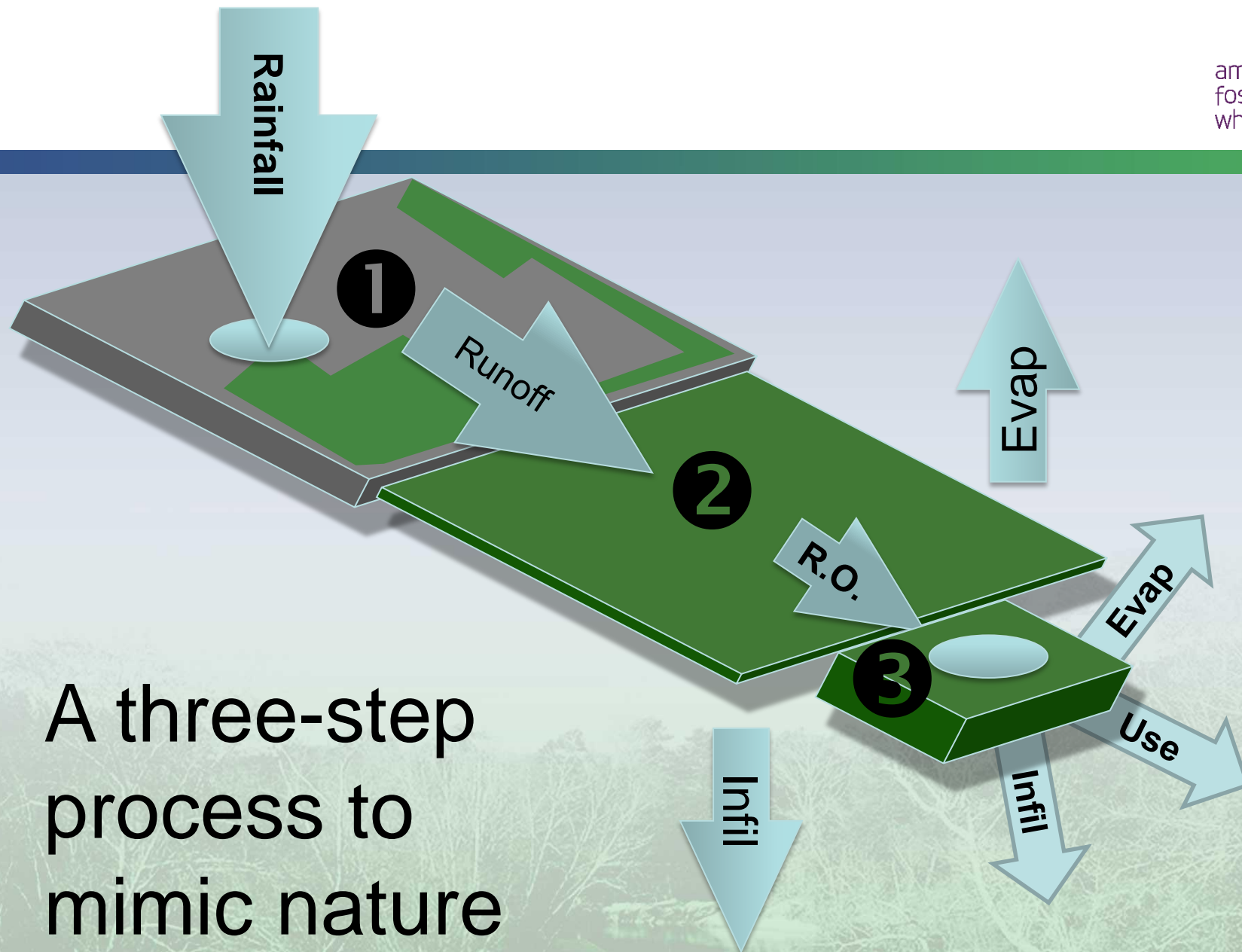
So...

- **A 1" storm is about 80% average annual volume capture**
- **C Soil with turf and some trees is about 80% average annual volume capture**
- **That is my back yard & streams in these areas are fairly stable and healthy**
- **GIPs can attain this 80% capture if appropriately sized to recognize underperformance rates**
- **ERGO: $R_v \leq 0.2$ is the single criterion we need and can encompass all these things**

Skip to the end...

If I can design a site with an average annual runoff of 20% I will both capture about an inch from all impervious area and mimic an acceptable urban hydrology looking like the typical Nashville back yard.

So if I can reliably assign annual R_v numbers to land uses and treatments (R_v out), insure conservatism, and close any technical loopholes I am there.



A three-step
process to
mimic nature

Tweaks:

- **Derivation across the state**
- **Controls in series**
- **Use with the 80% TSS approach**
- **Reduced CN for flood control**
- **Maximum size of IA before mandatory structural treatment (the golf course problem)**
- **Minimum distance from streams before mandatory structural treatment**



Table 2. Basic Land Uses

Step 1 Basic Land Use	CODE	Memphis	Nashville	Chattanooga	Knoxville	Tri-Cities
Target Rv		0.24	0.20	0.20	0.14	0.10
Basic Land Use	Impervious Surface IA	0.95	0.95	0.95	0.93	0.90
	Forest A Soil FA	0.02	0.02	0.02	0.01	0.01
	Forest B Soil FB	0.04	0.03	0.03	0.02	0.02
	Forest C Soil FC	0.05	0.04	0.04	0.03	0.02
	Forest D Soil FD	0.06	0.05	0.05	0.04	0.03
	Turf A Soil TA	0.18	0.15	0.15	0.11	0.08
	Turf B Soil TB	0.22	0.18	0.18	0.13	0.09
	Turf C Soil TC	0.24	0.20	0.20	0.14	0.10
	Turf D Soil TD	0.28	0.23	0.23	0.16	0.13

Table 3. Modified Land Uses

Step 1a Modified Land Use	CODE	Memphis	Nashville	Chattanooga	Knoxville	Tri-Cities
Natural or Amended Soil	A AA	0.03	0.03	0.03	0.02	0.01
	B AB	0.10	0.08	0.08	0.05	0.04
	C AC	0.16	0.13	0.13	0.09	0.07
	D AD	0.28	0.23	0.23	0.16	0.13
Urban Forest	A UA	0.12	0.10	0.10	0.07	0.05
	B UB	0.14	0.12	0.12	0.08	0.06
	C UC	0.16	0.13	0.13	0.09	0.07
	D UD	0.19	0.16	0.16	0.11	0.08
Reforestation	A RA	0.12	0.10	0.10	0.07	0.05
	B RB	0.14	0.12	0.12	0.08	0.06
	C RC	0.16	0.13	0.13	0.09	0.07
	D RD	0.192	0.16	0.16	0.112	0.08
	A Amended RAA	0.02	0.02	0.02	0.01	0.01
	B Amended RBA	0.04	0.03	0.03	0.02	0.02
	C Amended RCA	0.05	0.04	0.04	0.03	0.02
	D Amended RDA	0.06	0.05	0.05	0.04	0.03
Green Roof	Level 1 G1	0.24	0.20	0.20	0.14	0.10
	Level 2 G2	0.12	0.10	0.10	0.07	0.05

Step 2 Intrinsic RRP	CODE	Memphis	Nashville	Chattanooga	Knoxville	Tri-Cities
Downspout Disconnection	A/B Soil DAB	0.60	0.50	0.50	0.35	0.25
	C/D Soil DCD	0.84	0.75	0.75	0.53	0.38
	Amended DAS	0.60	0.50	0.50	0.35	0.25
Sheet Flow	Cons Area A/B SAB	0.30	0.25	0.25	0.18	0.13
	Cons Area C/D SCD	0.60	0.50	0.50	0.35	0.25
	Strip A SA	0.60	0.50	0.50	0.35	0.25
	Strip Amended SAS	0.60	0.50	0.50	0.35	0.25

Step 3 & 3a Structural RRP	CODE	Memphis	Nashville	Chattanooga	Knoxville	Tri-Cities
Permeable Pavement	Level 1 P1	0.66	0.55	0.55	0.39	0.28
	Level 2 P2	0.30	0.25	0.25	0.18	0.13
Grass Channel	A/B Soil GAB	0.88	0.80	0.80	0.56	0.40
	C/D Soil GCD	0.91	0.90	0.90	0.63	0.45
	A/B Amended GAA	0.81	0.70	0.70	0.49	0.35
	C/D amended GCA	0.88	0.80	0.80	0.56	0.40
Bioretention/ Rain Garden	Level 1 B1	0.48	0.40	0.40	0.28	0.20
	Level 2 B2	0.24	0.20	0.20	0.14	0.10
Water Quality Swales	Level 1 S1	0.70	0.60	0.60	0.42	0.30
	Level 2 S2	0.48	0.40	0.40	0.28	0.20
Infiltration Trench	Level 1 I1	0.60	0.50	0.50	0.35	0.25
	Level 2 I2	0.12	0.1	0.1	0.07	0.05
Urb Bioretention	UB	0.48	0.40	0.40	0.28	0.20
Dry Pond	D1	0.90	0.85	0.85	0.60	0.43
Cistern	CIS	Des. Dep.	Des. Dep.	Des. Dep.	Des. Dep.	Des. Dep.

Simple Spreadsheet Calcs

Percent Volume Reduction-Based Calculations

Step 1: Lay out the site and divide it into sub-areas each of a specific land use type and Rv.				Step 1a: Change any basic land use types through reforestation or green roofs - or through use of open space for a GIP.			Step 2: Treat impervious areas through the use of disconnection or sheet flow			Step 3: Treat primarily impervious areas with structural GIPs either in series with Step 3 intrinsic GIPs or alone downstream from Steps 1 and 2 land use.			Size controls for Step 3 by assigning structure ID to each sub-area, combining sub-areas into one structure if appropriate.			Step 3a Treatment in Series Calculation - Place Structural GIPs in same row as upstream GIP			Size controls for Step 3a in series by assigning a sequential structure ID to each area treated in series.		
Step1 Basic Land Use				Step 1a Modified LU			Step 2 Intrinsic GIPs			Step 3 Structural GIPs			Structure ID	IA Capture		Step 3a Structural GIPs in Series			Structure ID	IA Capture	
Subarea	Code	Acres	Base Rv	Code	Acres	Eff Rv1	Code	Trtmt VR1	Eff Rv2	Code	Trtmt VR2	Eff Rv3		Tv Multiplier	Tv (cf)	Code	Trtmt VR2	Eff Rv4		Tv Multiplier	Structure in Series Tv (cf)
1	IA	0.5	0.95	IA	0.5	0.95	SCD	0.5	0.48	B1	0.6	0.19		1.00	-		0	0.19		0.00	-
2	IA	0.4	0.95	RC	0.4	0.08		0	0.08	B1	0.6	0.04		1.00	-		0	0.04		0.00	-
3	IA	0.3	0.95	IA	0.3	0.95	SCD	0.5	0.48	B1	0.6	0.19		1.00	-		0	0.19		0.00	-
4	IA	0.2	0.95	IA	0.2	0.95		0	0.95	GCD	0.1	0.86		0.00	-		0	0.86		0.00	-
5			0.00		0	0.00		0	0.00		0	0.00		0.00	-		0	0.00		0.00	-
6			0.00		0	0.00		0	0.00		0	0.00		0.00	-		0	0.00		0.00	-
7			0.00		0	0.00		0	0.00		0	0.00		0.00	-		0	0.00		0.00	-
8			0.00		0	0.00		0	0.00		0	0.00		0.00	-		0	0.00		0.00	-
9			0.00		0	0.00		0	0.00		0	0.00		0.00	-		0	0.00		0.00	-
10			0.00		0	0.00		0	0.00		0	0.00		0.00	-		0	0.00		0.00	-
11			0.00		0	0.00		0	0.00		0	0.00		0.00	-		0	0.00		0.00	-
12			0.00		0	0.00		0	0.00		0	0.00		0.00	-		0	0.00		0.00	-
13			0.00		0	0.00		0	0.00		0	0.00		0.00	-		0	0.00		0.00	-
14			0.00		0	0.00		0	0.00		0	0.00		0.00	-		0	0.00		0.00	-
15			0.00		0	0.00		0	0.00		0	0.00		0.00	-		0	0.00		0.00	-
16			0.00		0	0.00		0	0.00		0	0.00		0.00	-		0	0.00		0.00	-
17			0.00		0	0.00		0	0.00		0	0.00		0.00	-		0	0.00		0.00	-
18			0.00		0	0.00		0	0.00		0	0.00		0.00	-		0	0.00		0.00	-
19			0.00		0	0.00		0	0.00		0	0.00		0.00	-		0	0.00		0.00	-
20			0.00		0	0.00		0	0.00		0	0.00		0.00	-		0	0.00		0.00	-
	Weighted Rv		0.95	Weighted Rv		0.701	Weighted Rv		0.430	Weighted Rv		0.243		Step 5 Tv Total	0			0.243		Final Tv Total	0
	Total Area 1.4		1.33	Total Area 1.4		0.98			0.60			0.34					0.34				
% Removal (Goal≥80%)-->			5.0%	% Removal		29.9%	% Removal		57.0%	% Removal		75.7%	% Removal			75.7%					

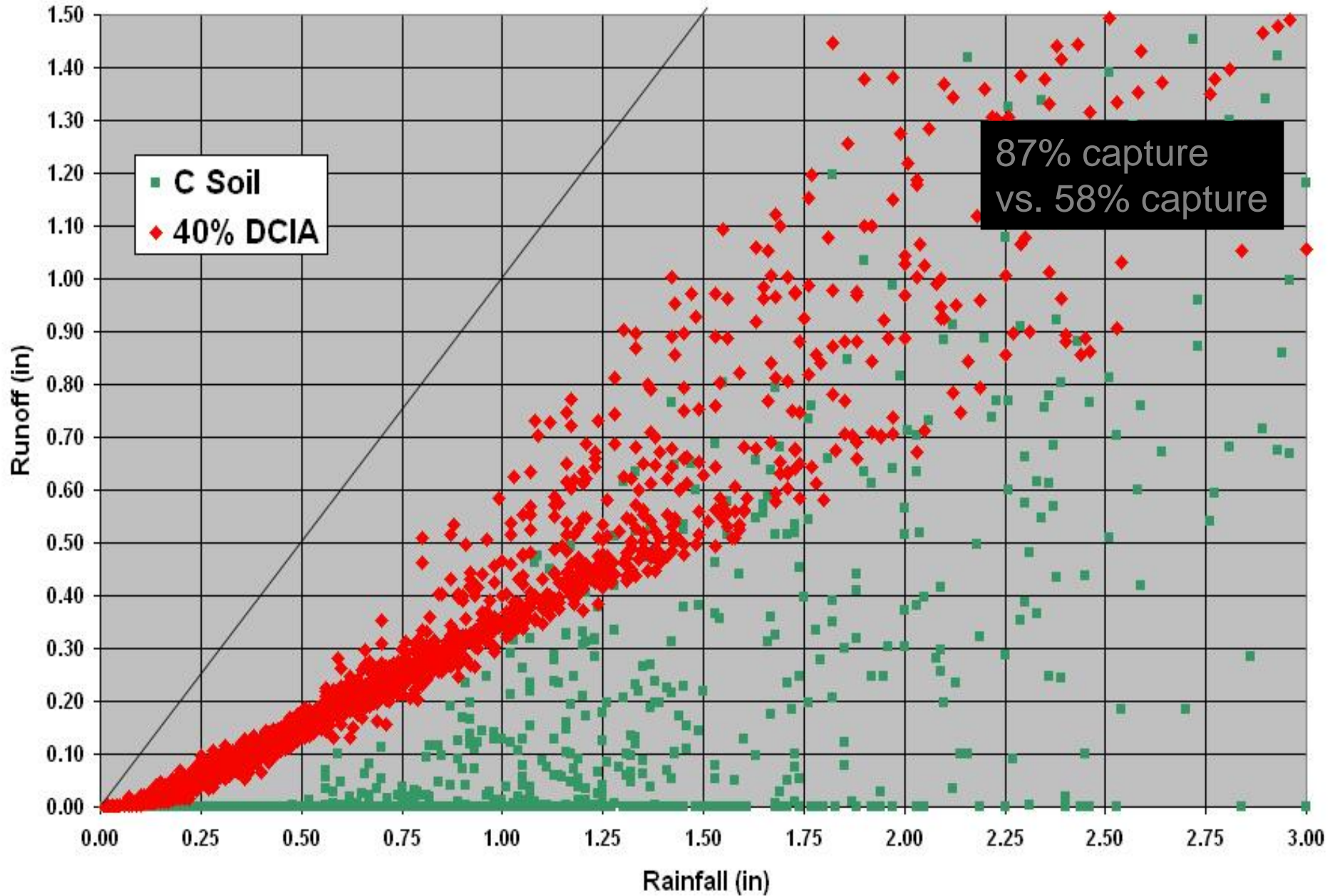
THIS MUST BE 80% OR GREATER
IT WILL TURN GREEN WHEN IT IS

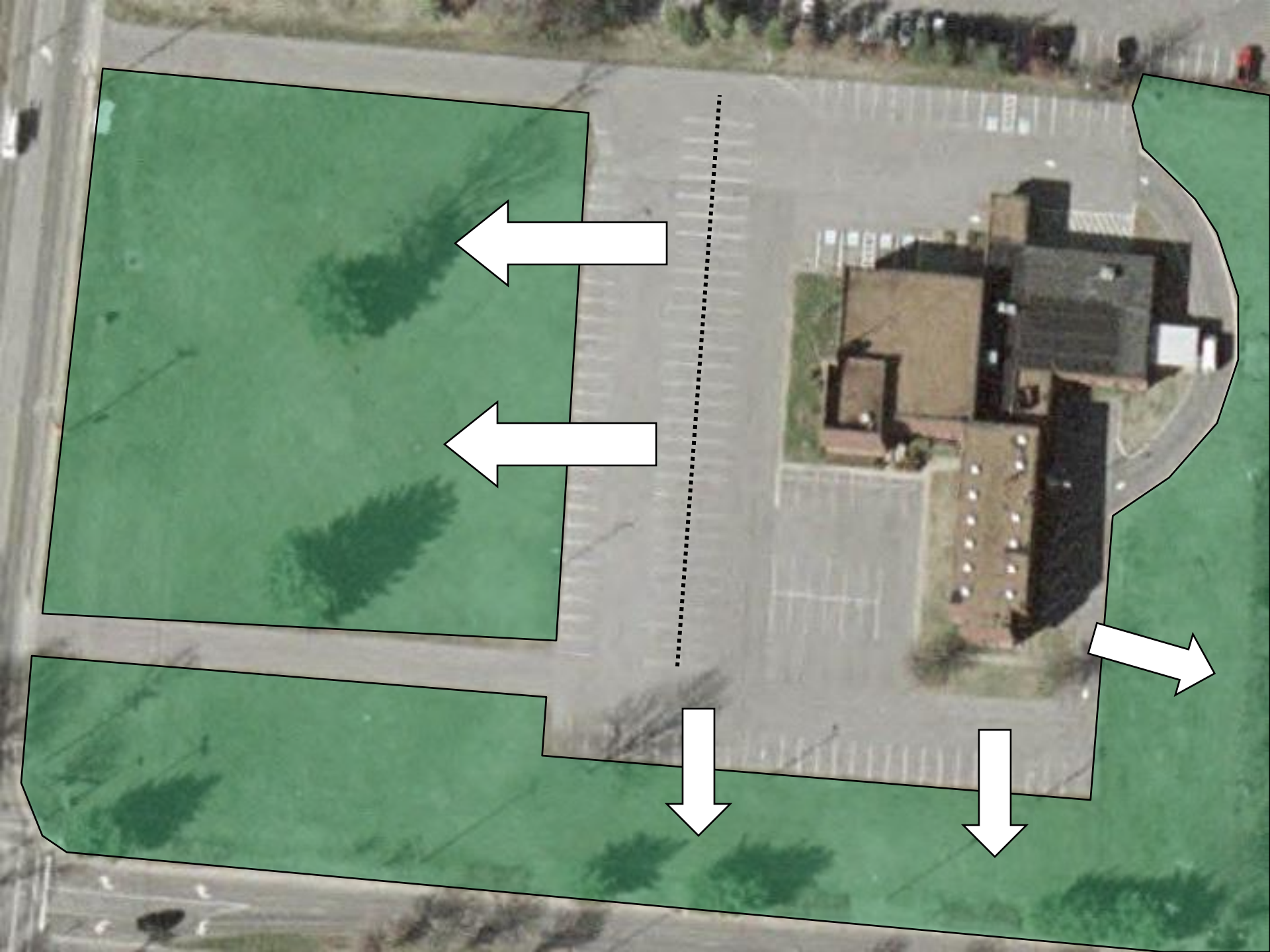
THIS MUST BE 80% OR GREATER
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40% Impervious DCIA

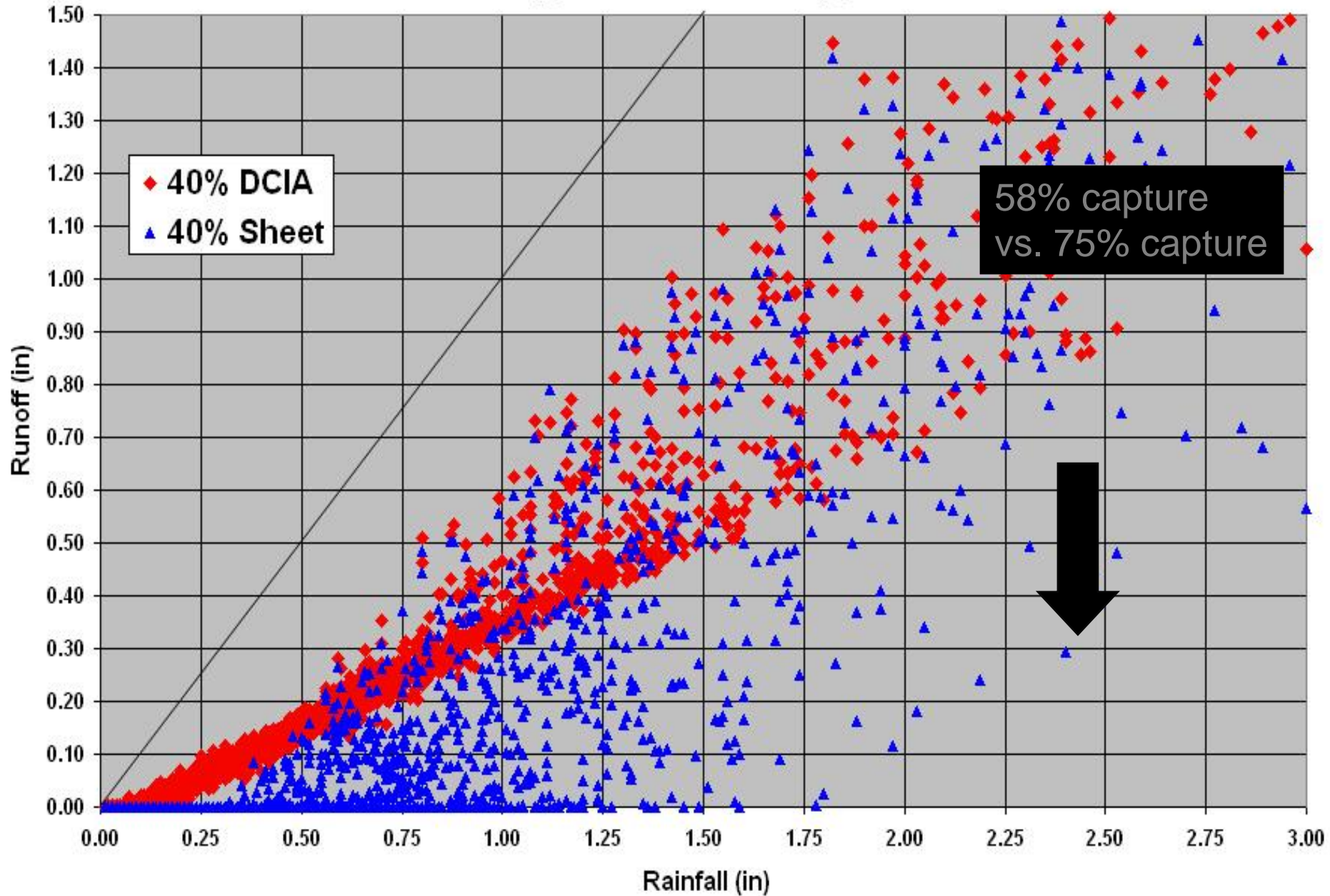


C Soil + 40% DCIA



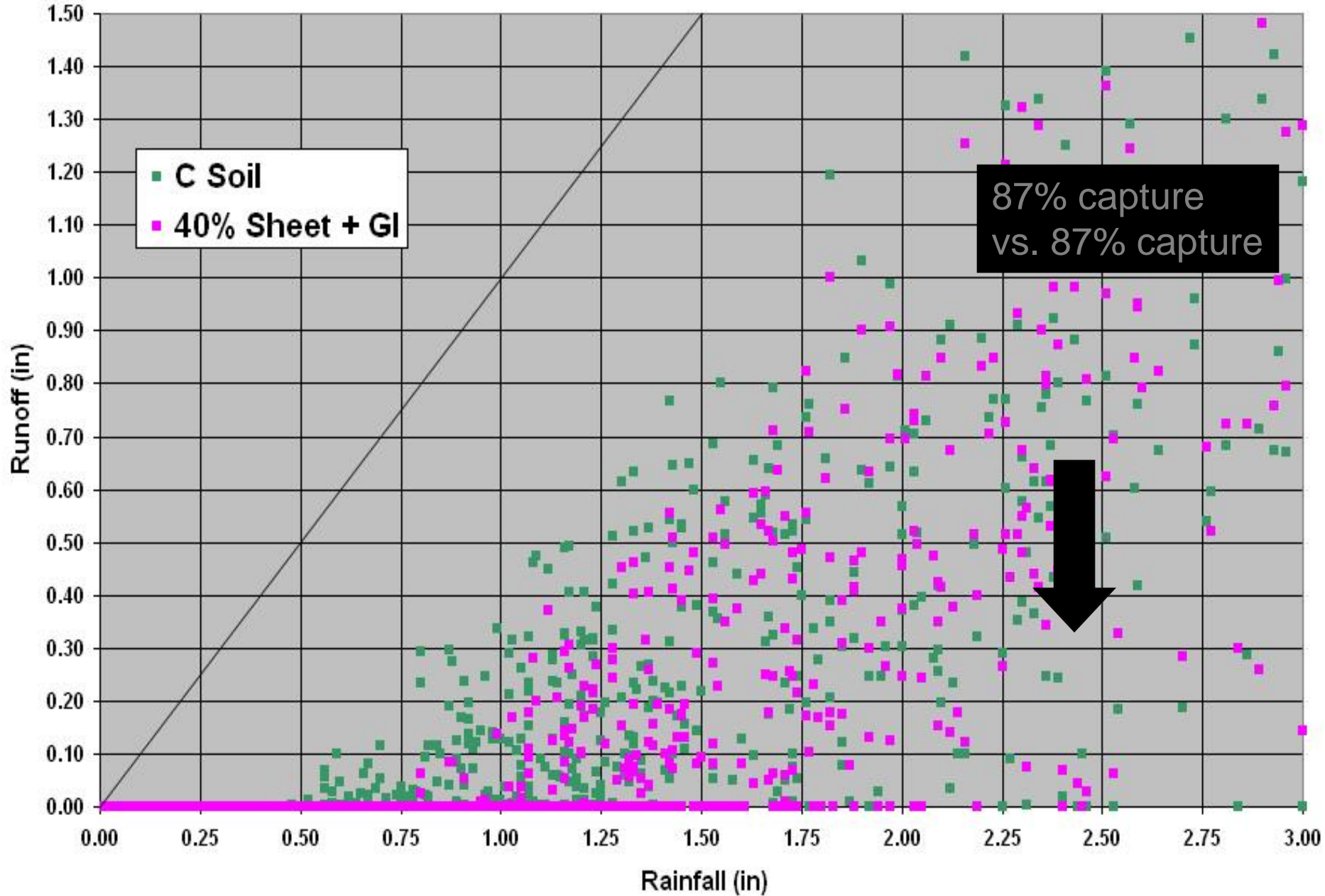


C Soil 40% DCIA & 40% Sheet



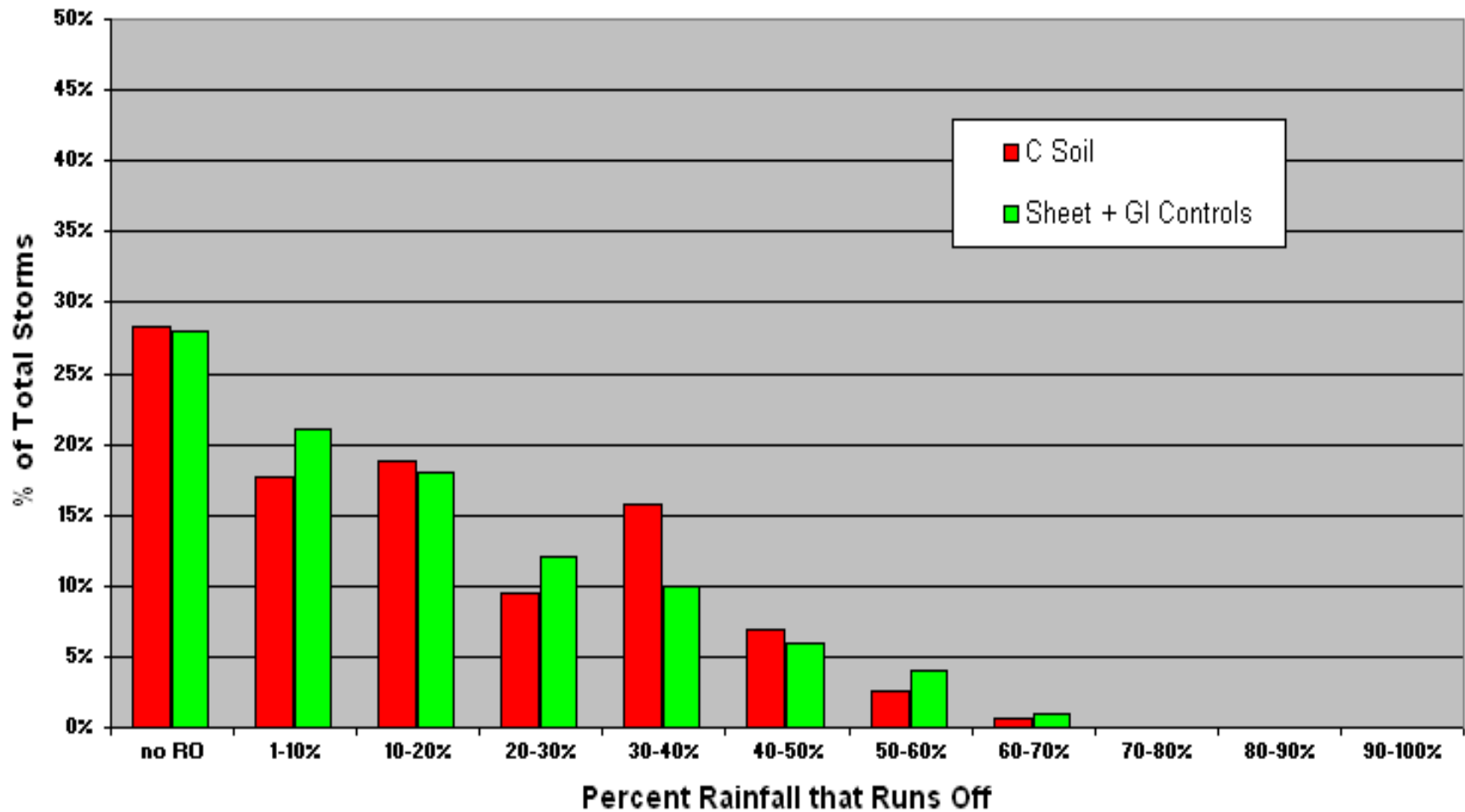


C Soil + Sheet Flow and Green Infrastructure



Steps to “Mimic Nature”

Modeled 95% Storm Runoff Characteristics
159 storms w/i 20% of the 95% Storm Depth, Nashville, TN



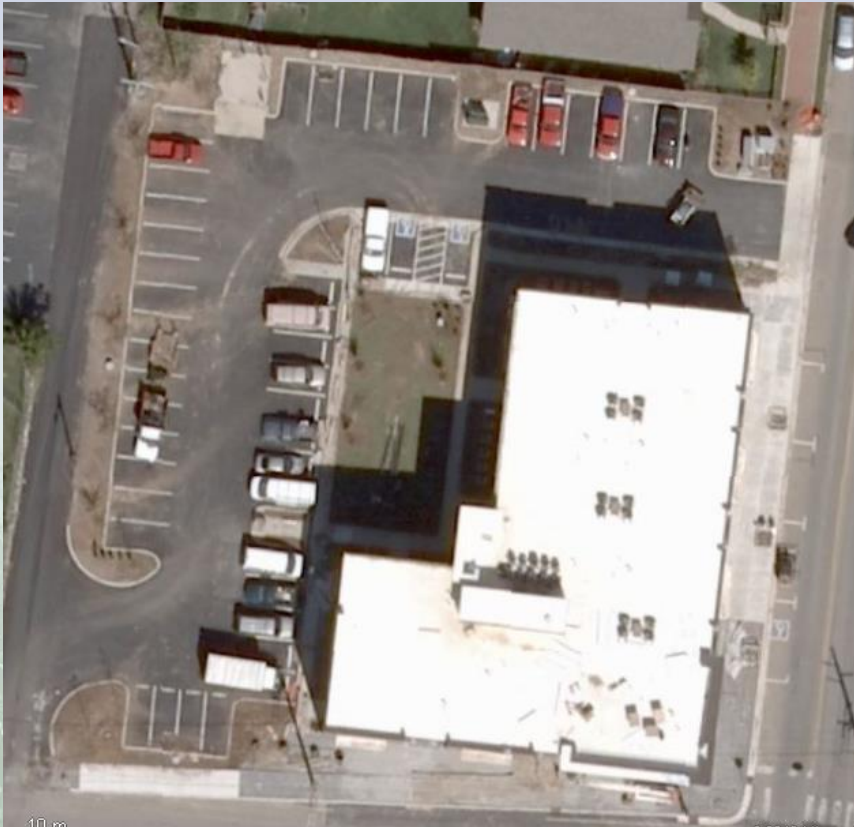
Meeting the Standard by Example



- **Site Area = 1 Acre**
- **Urban Setting**
- **Building Footprint = 26%**
- **Total Impervious = 86%**
- **Goal: Site composite of $R_v = 0.2$**

Calculate Site Weighted Rv

- Impervious = 0.86 Acres
- Turf C Soil = 0.14 Acres



Soil Condition	Volumetric Runoff Coefficient (Rv)			
Impervious Cover	0.95			
Hydrologic Soil Group	A	B	C	D
Forest Cover	0.02	0.03	0.04	0.05
Turf	0.15	0.18	0.20	0.23

$$Rv = \frac{[(0.86Ac)(0.95) + (0.14Ac)(0.2)]}{1Ac}$$

$$Rv = 0.85 >> 0.2$$

- Permeable Concrete (0.1 Ac)
- Bioretention (0.64 Ac)
- Green Roof (0.12 Ac)
- Turf C Soil (0.14 Ac)

$$R_v = \frac{(0.1 \text{ Ac} * 0.24) + (0.64 \text{ Ac} * 0.19) + (0.12 \text{ Ac} * 0.2) + (0.14 \text{ Ac} * 0.2)}{1 \text{ Ac}}$$

$$R_v = 0.198 < 0.2$$



Some potential advantages

- It is simple to understand and little harder than a “C” Factor calculation
- It balances data, experience, and continuous modeling
- It’s three steps value natural treatment approaches first
- It is derived for an area and thus does not force a one-size-fits-all criteria
- It integrates natural vegetation without a logic break
- It is appropriately conservative where real-world failure rates are known

Nashville to date:

- About 80 sites – generally successful
- Staff is in favor of the approach and feels it promotes its objectives and priorities
- About 25% of developers choose this approach over the older TSS approach
- It will become mandatory as the first line of water quality treatment next year

Questions?

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